

CITY OF WHITE SALMON
RESIDENTIAL PLAN REVIEW

PERMIT B2005-61



OWNER Steve Delaer
ADDRESS PO Box 671 Bingen, Wa
TELEPHONE 503-310-0319

CONTRACTOR self
LICENSE# DELAER*954NW
TELEPHONE same

SITE ADDRESS Gaddis Place

Engineer Charles Warren

SF: MAIN FLOOR 1535
2ND FLOOR _____
DECK 184

LWR FLR/BSMNT 875
GARAGE 545
OTHER _____

VALUATION \$216,555

ROOF LIVE LD 52 #PSF
FLOOR LIVE LD 40/30 #PSF
DECK LIVE LD 52 #PSF
WIND LOAD <110 mph Exposure
3 sec. Gust

GLAZING 11%
SOIL TYPE 1800
FROST DEPTH 18"
SEISMIC ZONE D-1
CONST TYPE V-B
OCCUPANCY R-3

ENGINEERED DESIGN Y N lower level only

FOOTING SIZE: See engn.
CONT. REBAR _____
VERT. REBAR _____

FOUNDATION: See engn.
CONT. REBAR _____
VERT. REBAR _____

ANCHORBOLTS:
PAGE _____
 4"OC 6"OC OTHER
Washers req. 1/4"X3"X3"

ABP: Y N
LOCATION _____
HOLDDOWNS _____

PORTAL FRAME: Y N
LOCATION _____
HOLDDOWNS _____

WALL SHEATHING: Continuous sheathed
SIZE 7/16" OSB
NAILING 8d 6"X12"

ROOF SHEATHING:
SIZE 1/2" ply
NAILING 8d @ 6"X12"

FLOORS:
SHEATHING 3/4"OSB
NAILING 10d @ 6"X12"

SPECIAL HOLD DOWNS:
PAGE _____
LOCATION _____
TYPE _____

CORRECTIONS/COMMENTS:

- 1- Main floor level detail to be provided prior to start of framing, main floor conventional wood frame 2"X6" OC studs
- 2- all structural headers to be minimum 4"X10" #2 doug fir(except garage provide size)
- 3- See continuous sheathed corner detail. 4- Verify Temp. glass locations. 5- Whole house ventilation system required
- 6- Maintain garage/ house fire separation

No modifications to this structure or any component shall be commenced without the approval of the Building Official.

PLANS REVIEWED BY Dean A. Nygaard

DATE 9/18/2005

Notice
Approved plans shall be
accompanied by the plan review
in order to be valid.

ADDRESS, PERMIT AND INSPECTION CARD MUST BE VISIBLE

Approved plans, plan review and engineering are required ON SITE at time of inspections.

Inspections: All requests must be received by 8:00am the day of the inspection. 24 hour request line 509-493-1133

- Foundation:
 - Site/Setbacks
 - Footings
 - Stemwalls
 - Monopour
 - Slab insulation
 - Appliance Protection/Slab
 - Seismic anchors
- Post & Beam:
 - Post & Beam/Underfloor
 - Epoxy anchorage
 - Roof Sheathing
 - Seismic Strapping
 - Wall Sheathing
 - Rough Electrical Labor & Ind.
 - Rough Plumbing
 - Rough Mechanical/Gas Piping
- Framing:
 - Framing
- Insulation:
 - Insulation/Windows
- Drywall:
 - Drywall
 - Firewall
- Final:
 - Final Structural
 - Fire Department Approval (Applicant must notify Fire Dept.)
 - Final Electrical - Labor & Ind.
 - Final Plumbing -
 - Final Mechanical



Please Note: Repeated failure to make required corrections may result in additional fees incurred for re-inspection.

FINAL INSPECTION IS REQUIRED PRIOR TO OCCUPANCY (No personal belongings, furniture, etc.)

Any changes to approved plans or site plan shall be submitted in writing. Approval must be signed on both sets of plans. Changes to Site Plan must be presented to Planning Dept. (See Land Use Conditions of Approval Letter.)

Expirations. Every permit issued shall become invalid unless the work authorized by such permit is commenced within 180 days after its issuance, or if the work authorized by such permit is suspended or abandoned for a period of 180 days after the time the work is commenced. The Building Official is authorized to grant, in writing, one or more extensions of time, for periods not more than 180 days each. The extension shall be requested in writing and justifiable cause demonstrated.

Inspection Requests. It shall be the duty of the person doing the work authorized by the permit to notify the Building Official that such work is ready for inspection. It shall be the duty of the person requesting any inspections required by this code to provide access to and means for inspection of such work.

Approval Required. Work shall not be done beyond the point indicated in each successive inspection without first obtaining the approval of the Building Official. The Building Official upon notification shall make the requested inspections and shall either indicate the portion of the construction that is satisfactory as completed, or shall notify the permit holder or an agent of the permit holder wherein the same fails to comply with this code. Any portions that do not comply shall be corrected and such portions shall not be covered or concealed until authorized by the Building Official.

The issuance of a permit shall not prevent the correction of errors in plans, specifications or the construction.

Print Name _____

Signature _____ Date _____

NOTE: 2004.2 Allowable Stress Design

- THIS COMPONENT IS DESIGNED TO SUPPORT ONLY THE VERTICAL LOADS SHOWN VERIFICATION OF LOADING, DEFLECTION LIMITATIONS, FRAMING METHODS, WIND AND SEISMIC BRACING, AND OTHER LATERAL BRACING THAT IS ALWAYS REQUIRED BY THE RESPONSIBILITY OF THE PROJECT ENGINEER OR ARCHITECT.
- PROVIDE RESTRAINT AT SUPPORTS TO ENSURE LATERAL STABILITY.
- DO NOT CUT, NOTCH OR DRILL LPI FLANGES.
- SHIM ALL BEARINGS FOR FULL CONTACT.
- VERIFY DIMENSIONS BEFORE CUTTING LPI TO SIZE.
- THIS LPI IS TO BE USED AS A FLOOR JOIST ONLY.
- PROVIDE COMPRESSION EDGE BRACING AT 27' O.C. OR LESS.

LOAD TABLE

NOTE: LOADS SHOWN ARE FOR INPUT LOAD CASE (1). OTHER LOAD CASES FOR PATTERN LIVE LOADING ARE CHECKED AS REQUIRED. (DIMENSIONS MEASURED FROM LEFT END OF SPAN OR CANTILEVER.)

DISTRIBUTION	SOURCE TYPE	TOP/SIDE	LOAD	FROM	TO	LOAD
UNIFORM	FLOOR LIVE	TOP	53 PLF	FT-IN-SX	FT-IN-SX	LDF
UNIFORM	FLOOR DEAD	TOP	20 PLF	00-00-00	31-06-04	1.00
				00-00-00	31-06-04	0.90

WARNING NOTES:

THIS COMPONENT DESIGN IS SPECIFICALLY FOR L-P ENGINEERED WOOD PRODUCTS. USE OF THIS DESIGN FOR ANYTHING OTHER THAN GANG-LAM LVL OR LPI JOISTS IS STRICTLY PROHIBITED. ANY MODIFICATION OF THIS DOCUMENT REQUIRES REVIEW BY A DESIGN PROFESSIONAL.

MINIMUM BEARING SIZES ARE SUFFICIENT TO PREVENT CRUSHING OF THE LPI JOIST AS DESIGNED. IT IS THE RESPONSIBILITY OF THE PROJECT ENGINEER, ARCHITECT OR DESIGNER TO VERIFY THAT THE SUPPORT STRUCTURE FOR THIS BEAM IS CAPABLE OF SUPPORTING THE REACTIONS.

ANCHOR LPI JOIST SECURELY TO BEARINGS OR HANGERS.

DESIGN CRITERIA : MSI: 0.62 VSI: 0.56
 LIVE LOAD = 40 PSF
 DEAD LOAD = 15 PSF
 TOTAL LOAD = 55 PSF
 SPACING = 16.00 IN. C/C

DEFLECTION CRITERIA :
 LIVE LOAD DEFL: L / 480
 TOTAL LOAD DEFL: L / 240

LOAD SHARING: 7

CODE COMPLIANCES :
 REPORT #
 ICC-ES ESR-1305
 WISCONSIN 200405-W
 CCMC 12724-R

DEFLECTION ASSUMES COMPOSITE ACTION WITH GLUED AND NAILLED 23/32" APA RATED SHEATHING (48/24 SPAN RATING)

1 LPI 20W DEPTH 11.875"
 WES: 0.375"
 FLANGE 1.60 X 2.60

SUPPORT REACTIONS (LBS) :

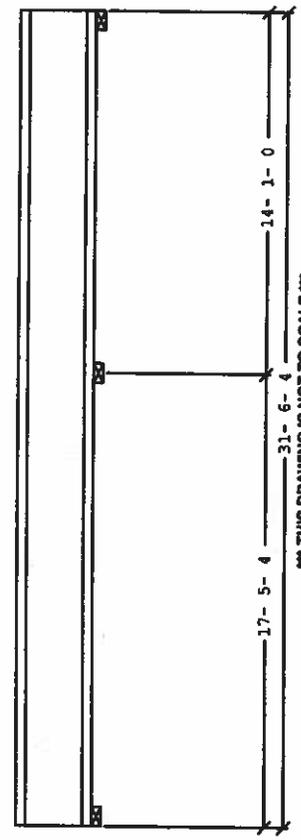
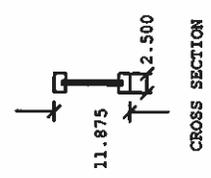
CASE	BEARING	NUMBER
1	504	1458
2	138	398
3	538	1007
4	104	849

MIN BEARING SIZES (IN-SX)

4-8	7-8	4-8
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MAXIMUM DEFLECTIONS

LIVE LOAD	0.21"
DEAD LOAD	0.09"
TOTAL LOAD	0.27"
	0.86"



Handling & Erection

Temporary and permanent bracing for holding component plumb and for resisting lateral forces shall be designed and installed by others. No loads are to be applied to the component until after all the framing and bracing are completed. At no time shall loads greater than design loads be applied to the component.

Design Criteria

The design and material specified are in substantial conformity with the latest provisions of NDS and AITC. Dead load deflection includes adjustment factor for creep. Total load deflection is instantaneous.

Miscellaneous Information

The use of this component shall be specified by the designer of the complete structure. Obtain all the necessary code compliance approval and instructions from the designers of the complete structure before using this component. If the design criteria listed above does not meet local building code requirements, do not use this design. When this drawing is signed and sealed, the structural design is approved as shown in this drawing based on data provided by the customer, Gang-Lam LVL and CTR. LPI joists are made without camber and will deflect under load. Wood in direct contact with concrete must be protected as required by code. Continuous lateral support is assumed (wall, floor beam, etc.). LP does not provide on-site inspection. This drawing must have an Architect's or Engineer's seal affixed to be considered an Engineering document.

Gang-Lam LVL and CTR, LPI Joist Specifications

- Supports and connections for Gang-Lam LVL and CTR, LPI Joists to be specific applications.
- Chairs driven parallel to glue lines shall be spaced a minimum of 6" for 10d and 3" for 4d.
- Do not cut, notch, drill or alter Gang-Lam LVL and CTR, LPI Joists except as shown in which are from LP any use of Gang-Lam LVL and CTR, LPI Joists contrary to the limits set forth herein requires any express warranty of the product and LP decisions all involved. LP does not include the implied warranties of merchantability and fitness for a particular use.

A COPY OF THIS DRAWING IS TO BE GIVEN TO THE INSTALLING CONTRACTOR LP is a registered trademark of Louisiana-Pacific Corporation.

Software Provided By:
 LP Engineered Wood Products
 2706 Highway 421 North
 Wilmington, NC 28401
 Local 910.762.8878
 National Wets 800.968.9105

07/21/05 IC80

DWG # _____
 SHEET # _____



CHARLES WARREN ENGINEERING

September 9, 2005

Steve Delaere
PO Box 671
Bingen, WA 98605

Cel (503) 310-0319

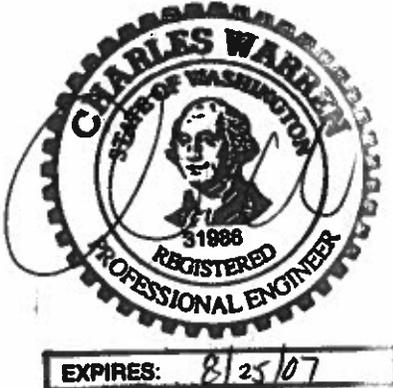
Re: Residence Retaining Walls for Gaddis Place

Steve;

Attached are design and calculation sheets for the residence retaining walls. The retaining walls for the house utilize the AMVIC Building System form blocks while the driveway retaining wall will be a conventional 8" thick wood formed wall.

If there are any questions please call.

Sincerely;



Charlie Warren, P.E.

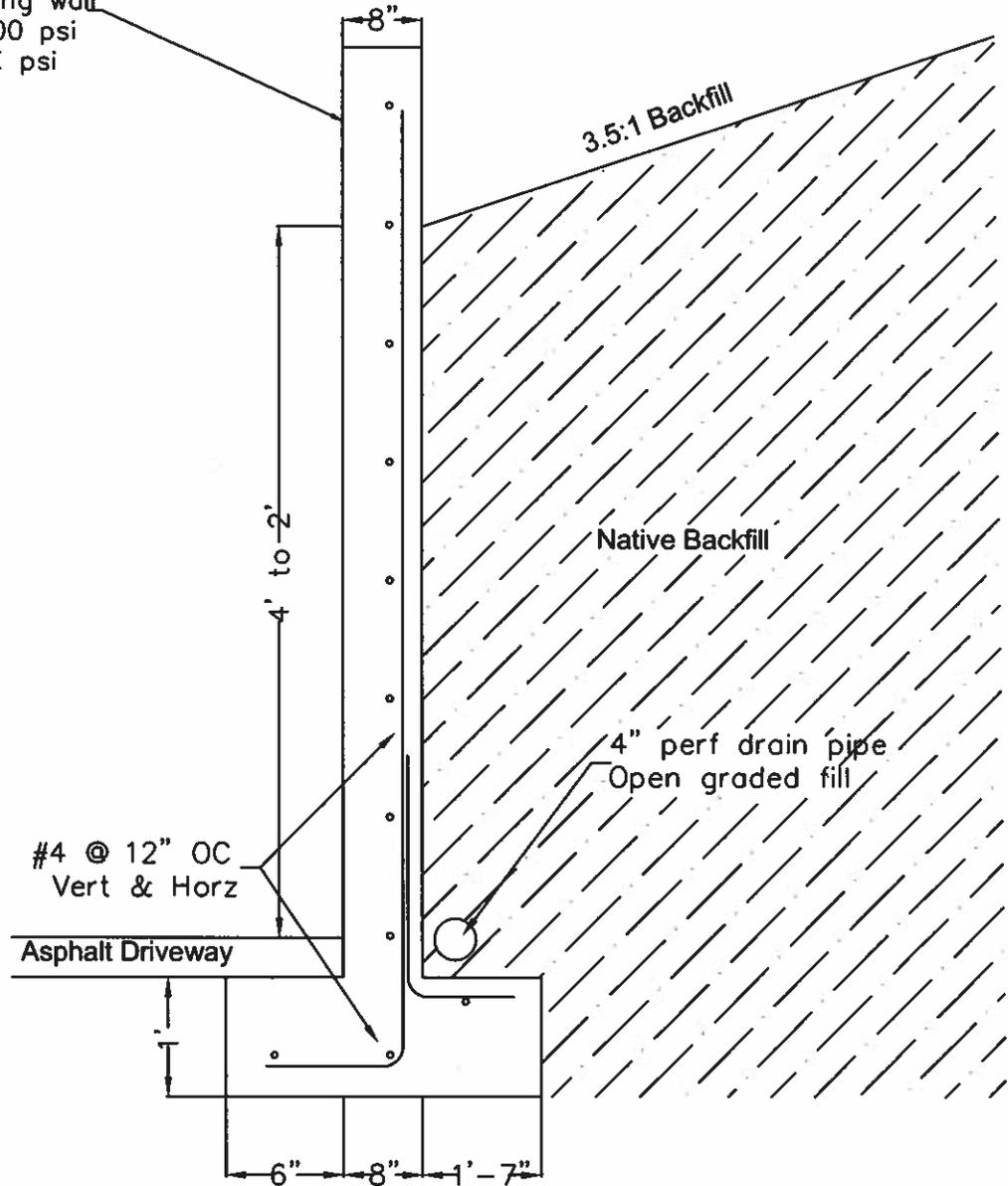
Attach: Drawing & Calculation Sheets



CHARLES WARREN ENGINEERING

409 Montello Ave. Hood River, OR Ph (541) 386-1455 FAX (541) 386-1322
engs@gorge.net

Proposed 4' to 6' retaining wall
F'c Concrete = 3,000 psi
Fy Steel = 60K psi

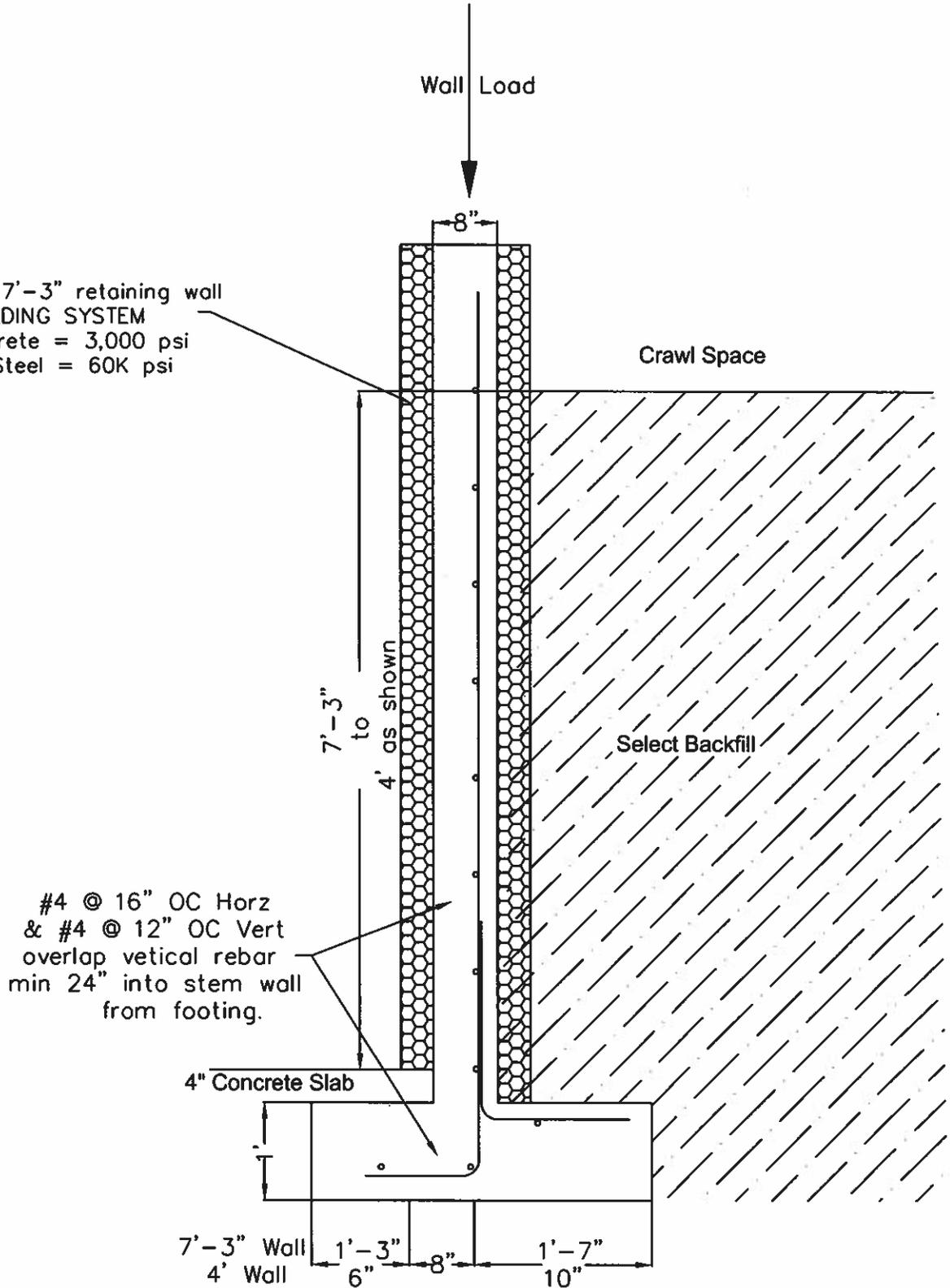


DELAERE DRIVEWAY RETAINING WALL DETAIL

GADDIS PLACE, WHITE SALMON
NO SCALE



Proposed 4' to 7'-3" retaining wall
Use AMVIC BUILDING SYSTEM
F'c Concrete = 3,000 psi
Fy Steel = 60K psi

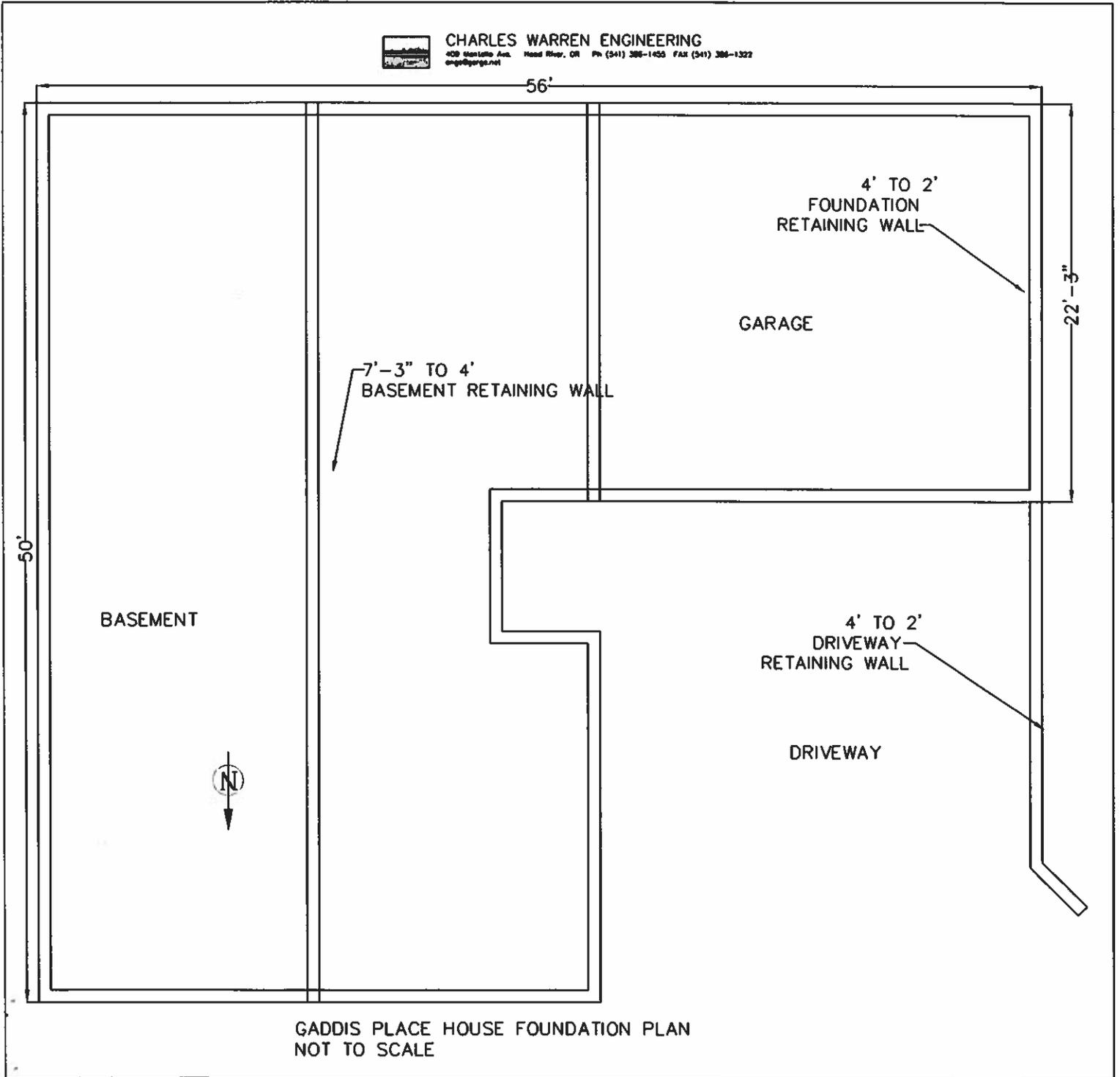


DELAERE BASEMENT RETAINING WALL DETAIL

GADDIS PLACE, WHITE SALMON
NO SCALE



CHARLES WARREN ENGINEERING
409 Mantoloking Ave. Hood River, OR Ph (541) 386-1455 FAX (541) 386-1322
engr@cweng.net



GADDIS PLACE HOUSE FOUNDATION PLAN
NOT TO SCALE



CHARLES WARREN ENGINEERING
 409 Montello Ave.
 Hood River, OR 97031
 (541) 386-1455

Title : **Delaere Gaddis Place**
 Job # : **29.05** Dsgnr: **CW**
 Description....
4' Driveway retaining wall

Page: _____
 Date: **SEP 8,2005**

This Wall in File: c:\rp6\projects\delaaere gaddis place.rp5

RetainPro Version 6.0

Build Date : 10-SEP-2001, (c) 1989-2001

Cantilevered Retaining Wall Design

Criteria	Soil Data	Footing Dimensions & Strengths
Retained Height = 4.00 ft	Allow Soil Bearing = 2,000.0 psf	Toe Width = 0.50 ft
Wall height above soil = 0.50 ft	Equivalent Fluid Pressure Method	Heel Width = 2.25
Slope Behind Wal = 3.50 : 1	Heel Active Pressure = 30.0 psf/ft	Total Footing Width = 2.75
Height of Soil over Toe = 4.00 in	Toe Active Pressure = 30.0 psf/ft	Footing Thickness = 12.00 in
Soil Density = 120.00 pcf	Passive Pressure = 250.0 psf/ft	Key Width = 0.00 in
Wind on Stem = 0.0 psf	Water height over heel = 1.0 ft	Key Depth = 0.00 in
	Footing Soil Frictior = 0.400	Key Distance from Toe = 0.00 ft
	Soil height to ignore for passive pressure = 12.00 in	f _c = 3,000 psi F _y = 60,000 psi
		Footing Concrete Density = 150.00 pcf
		Min. As % = 0.0018
		Cover @ Top = 2.00 in @ Btm. = 3.00 in
		Axial Load Eccentricity = 0.0 in

Axial Load Applied to Stem

Axial Dead Load = 50.0 lbs
 Axial Live Load = 10.0 lbs

Design Summary

Total Bearing Load = 1,745 lbs
 ...resultant ecc. = 4.68 in

Soil Pressure @ Toe = 1,174 psf OK
 Soil Pressure @ Heel = 95 psf OK
 Allowable Soil Pressure Less Than Allowable = 2,000 psf

ACI Factored @ Toe = 1,646 psf
 ACI Factored @ Heel = 133 psf

Footing Shear @ Toe = 0.0 psi OK
 Footing Shear @ Heel = 4.9 psi OK
 Allowable = 93.1 psi

Wall Stability Ratios
 Overturning = 2.99 OK
 Sliding = 1.54 OK

Sliding Calcs (Vertical Component NOT Used)
 Lateral Sliding Force = 512.9 lbs
 less 100% Passive Force = - 97.2 lbs
 less 100% Friction Force = - 694.2 lbs

Added Force Req'd = 0.0 lbs OK
for 1.5 : 1 Stability = 0.0 lbs OK

Stem Construction

Design height ft = 0.00
 Wall Material Above "Ht" = Concrete
 Thickness = 8.00
 Rebar Size = # 4
 Rebar Spacing = 12.00
 Rebar Placed at = Edge

Design Data
 fb/FB + fa/Fa = 0.102
 Total Force @ Section lbs = 444.9
 Moment....Actual ft-# = 556.9
 Moment.....Allowable = 5,448.0
 Shear.....Actual psi = 5.9
 Shear.....Allowable psi = 93.1
 Lap Splice if Above in = 28.48
 Lap Splice if Below in = 7.67
 Wall Weight = 100.0
 Rebar Depth 'd' in = 6.25

Top Stem

Stem OK

Masonry Data

f_m psi =
 F_s psi =
 Solid Grouting =
 Special Inspection =
 Modular Ratio 'n' =
 Short Term Factor =
 Equiv. Solid Thick. =
 Masonry Block Type = Medium Weight

Concrete Data

f_c psi = 3,000.0
 F_y psi = 60,000.0

Other Acceptable Sizes & Spacings

Toe: Not req'd, Mu < S * Fr
 Heel: Not req'd, Mu < S * Fr
 Key: No key defined

Footing Design Results

	Toe	Heel
Factored Pressure	1,646	133 psf
Mu' : Upward	194	0 ft-#
Mu' : Downward	33	0 ft-#
Mu: Design	161	557 ft-#
Actual 1-Way Shear	0.00	4.88 psi
Allow 1-Way Shear	93.11	93.11 psi
Toe Reinforcing	# 4 @ 12.00 in	
Heel Reinforcing	# 4 @ 12.00 in	
Key Reinforcing	None Spec'd	



CHARLES WARREN ENGINEERING
 409 Montello Ave.
 Hood River, OR 97031
 (541) 386-1455

Title : Delaere Gaddis Place
 Job # : 29.05 Dsgnr: CW
 Description....
 4' Driveway retaining wall

Page: _____
 Date: SEP 8, 2005

This Wall In File: c:\rp6\projects\delaware gaddis place.rp5

RetainPro Version 6.0

Build Date : 10-SEP-2001, (c) 1989-2001

Cantilevered Retaining Wall Design

Summary of Overturning & Resisting Forces & Moments

ItemOVERTURNING.....			=RESISTING.....		
	Force lbs	Distance ft	Moment ft-#		Force lbs	Distance ft	Moment ft-#
Heel Active Pressure	= 539.5	1.62	872.9	Soil Over Heel	= 760.0	1.96	1,488.3
Toe Active Pressure	= -26.7	0.44	-11.9	Sloped Soil Over Heel	= 43.0	2.22	95.5
Surcharge Over Toe	=			Surcharge Over Heel	=		
Adjacent Footing Load	=			Adjacent Footing Load	=		
Added Lateral Load	=			Axial Dead Load on Stem	= 50.0	0.83	41.7
Load @ Stem Above Soil	=			Soil Over Toe	= 20.0	0.25	5.0
				Surcharge Over Toe	=		
				Stem Weight(s)	= 450.0	0.83	375.0
				Earth @ Stem Transitions	=		
Total	= 512.9	O.T.M. =	861.0	Footing Weight	= 412.5	1.38	567.2
Resisting/Overturning Ratio		=	2.99	Key Weight	=		
Vertical Loads used for Soil Pressure	=	1,745.5 lbs		Vert. Component	=		
Vertical component of active pressure NOT used for soil pressure				Total =	1,735.5 lbs	R.M. =	2,572.7



CHARLES WARREN ENGINEERING
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Title : Delaere Gaddis Place
 Job # : 29.05 Dsgnr: CW Page: _____
 Date: SEP 8, 2005
 Description...
7'-3" HOUSE BASEMENT RETAINING WALL

This Wall in File: c:\rp6\projects\delaware gaddis place.rp5

RetainPro Version 6.0

Build Date : 10-SEP-2001, (c) 1989-2001

Cantilevered Retaining Wall Design

Criteria

Retained Height = 7.33 ft
 Wall height above soil = 1.50 ft
 Slope Behind Wal = 0.00 : 1
 Height of Soil over Toe = 4.00 in
 Soil Density = 120.00 pcf
 Wind on Stem = 0.0 psf

Soil Data

Allow Soil Bearing = 2,000.0 psf
 Equivalent Fluid Pressure Method
 Heel Active Pressure = 30.0 psf/ft
 Toe Active Pressure = 30.0 psf/ft
 Passive Pressure = 250.0 psf/ft
 Water height over heel = 1.0 ft
 Footing|Soil Frictior = 0.400
 Soil height to ignore for passive pressure = 12.00 in

Footing Dimensions & Strengths

Toe Width = 1.25 ft
 Heel Width = 2.25
 Total Footing Width = 3.50
 Footing Thickness = 12.00 in
 Key Width = 0.00 in
 Key Depth = 0.00 in
 Key Distance from Toe = 0.00 ft
 f_c = 3,000 psi F_y = 60,000 psi
 Footing Concrete Density = 150.00 pcf
 Min. As % = 0.0018
 Cover @ Top = 2.00 in @ Btm. = 3.00 in
 Axial Load Eccentricity = 0.0 in

Axial Load Applied to Stem

Axial Dead Load = 200.0 lbs
 Axial Live Load = 100.0 lbs

Design Summary

Total Bearing Load = 3,151 lbs
 ...resultant ecc. = 7.08 in
 Soil Pressure @ Toe = 1,811 psf OK
 Soil Pressure @ Heel = 0 psf OK
 Allowable Soil Pressure Less Than Allowable = 2,000 psf
 ACI Factored @ Toe = 2,553 psf
 ACI Factored @ Heel = 0 psf
 Footing Shear @ Toe = 11.1 psi OK
 Footing Shear @ Heel = 12.2 psi OK
 Allowable = 93.1 psi
Wall Stability Ratios
 Overturning = 2.19 OK
 Sliding = 1.19 Ratio < 1.5!
Sliding Calcs Slab Resists All Sliding !
 Lateral Sliding Force = 1,107.8 lbs

Stem Construction

Design height ft = 0.00
 Wall Material Above "Ht" = Concrete
 Thickness = 8.00
 Rebar Size = # 4
 Rebar Spacing = 12.00
 Rebar Placed at = Edge

Top Stem

Design Data
 fb/FB + fa/Fa = 0.617
 Total Force @ Section lbs = 1,407.0
 Moment....Actual ft-# = 3,360.5
 Moment....Allowable = 5,448.0
 Shear....Actual psi = 18.8
 Shear....Allowable psi = 93.1
 Lap Splice if Above in = 28.48
 Lap Splice if Below in = 7.67
 Wall Weight = 100.0
 Rebar Depth 'd' in = 6.25

Masonry Data

f_m psi =
 F_s psi =
 Solid Grouting =
 Special Inspection =
 Modular Ratio 'n' =
 Short Term Factor =
 Equiv. Solid Thick. =
 Masonry Block Type = Medium Weight

Concrete Data

f_c psi = 3,000.0
 F_y psi = 60,000.0

Other Acceptable Sizes & Spacings

Toe: Not req'd, Mu < S * Fr
 Heel: Not req'd, Mu < S * Fr
 Key: No key defined

Footing Design Results

	Toe	Heel
Factored Pressure	2,553	0 psf
Mu' : Upward	1,755	467 ft-#
Mu' : Downward	208	1,807 ft-#
Mu: Design	1,548	1,340 ft-#
Actual 1-Way Shear	11.09	12.16 psi
Allow 1-Way Shear	93.11	93.11 psi
Toe Reinforcing	# 4 @ 12.00 in	
Heel Reinforcing	# 4 @ 12.00 in	
Key Reinforcing	None Spec'd	



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Title : Delaere Gaddis Place
 Job # : 29.05 Dsgnr: CW Page: _____
 Date: SEP 8,2005
 Description....
 7'-3" HOUSE BASEMENT RETAINING WALL

This Wall in File: c:\rp6\projects\delaware gaddis place.rp5

RetainPro Version 6.0

Build Date : 10-SEP-2001, (c) 1989-2001

Cantilevered Retaining Wall Design

Summary of Overturning & Resisting Forces & Moments

ItemOVERTURNING.....			=RESISTING.....		
	Force lbs	Distance ft	Moment ft-#		Force lbs	Distance ft	Moment ft-#
Heel Active Pressure	= 1,134.4	2.60	2,952.4	Soil Over Heel	= 1,392.7	2.71	3,771.9
Toe Active Pressure	= -26.7	0.44	-11.9	Sloped Soil Over Heel	=		
Surcharge Over Toe	=			Surcharge Over Heel	=		
Adjacent Footing Load	=			Adjacent Footing Load	=		
Added Lateral Load	=			Axial Dead Load on Stem	= 200.0	1.58	316.7
Load @ Stem Above Soil	=			Soil Over Toe	= 50.0	0.63	31.3
				Surcharge Over Toe	=		
Total	= 1,107.8	O.T.M. =	2,940.6	Stem Weight(s)	= 883.0	1.58	1,398.1
Resisting/Overturning Ratio		=	2.19	Earth @ Stem Transitions	=		
Vertical Loads used for Soil Pressure	=	3,150.7 lbs		Footing Weight	= 525.0	1.75	918.8
Vertical component of active pressure NOT used for soil pressure				Key Weight	=		
				Vert. Component	=		
				Total =	3,050.7 lbs	R.M. =	6,436.6



RetainPro Version 6.0

Build Date : 10-SEP-2001, (c) 1989-2001

Cantilevered Retaining Wall Design

Criteria

Retained Height = 4.33 ft
 Wall height above soil = 1.50 ft
 Slope Behind Wal = 0.00 : 1
 Height of Soil over Toe = 4.00 in
 Soil Density = 120.00 pcf
 Wind on Stem = 0.0 psf

Soil Data

Allow Soil Bearing = 2,000.0 psf
 Equivalent Fluid Pressure Method
 Heel Active Pressure = 30.0 psf/ft
 Toe Active Pressure = 30.0 psf/ft
 Passive Pressure = 250.0 psf/ft
 Water height over heel = 1.0 ft
 Footing||Soil Frictior = 0.400
 Soil height to ignore for passive pressure = 12.00 in

Footing Dimensions & Strengths

Toe Width = 0.50 ft
 Heel Width = 1.50
 Total Footing Width = 2.00
 Footing Thickness = 12.00 in
 Key Width = 0.00 in
 Key Depth = 0.00 in
 Key Distance from Toe = 0.00 ft
 fc = 3,000 psi Fy = 60,000 psi
 Footing Concrete Density = 150.00 pcf
 Min. As % = 0.0018
 Cover @ Top = 2.00 in @ Btm. = 3.00 in
 Axial Load Eccentricity = 0.0 in

Axial Load Applied to Stem

Axial Dead Load = 200.0 lbs
 Axial Live Load = 100.0 lbs

Design Summary

Total Bearing Load = 1,636 lbs
 ...resultant ecc. = 5.26 in
 Soil Pressure @ Toe = 1,942 psf OK
 Soil Pressure @ Heel = 0 psf OK
 Allowable Soil Pressure Less Than Allowable = 2,000 psf
 ACI Factored @ Toe = 2,755 psf
 ACI Factored @ Heel = 0 psf
 Footing Shear @ Toe = 0.0 psi OK
 Footing Shear @ Heel = 4.9 psi OK
 Allowable = 93.1 psi
Wall Stability Ratios
 Overturning = 2.03 OK
 Sliding = 1.44 Ratio < 1.5!
Sliding Calcs Slab Resists All Sliding !
 Lateral Sliding Force = 493.1 lbs

Stem Construction

Design height ft = 0.00
 Wall Material Above "Ht" = Concrete
 Thickness = 8.00
 Rebar Size = # 4
 Rebar Spacing = 12.00
 Rebar Placed at = Edge
Design Data
 fb/FB + fa/Fa = 0.129
 Total Force @ Section lbs = 515.0
 Moment....Actual ft-# = 703.0
 Moment....Allowable = 5,448.0
 Shear....Actual psi = 6.9
 Shear....Allowable psi = 93.1
 Lap Splice if Above in = 28.48
 Lap Splice if Below in = 7.67
 Wall Weight = 100.0
 Rebar Depth 'd' in = 6.25

Top Stem

Stem OK

Masonry Data

f'm psi =
 Fs psi =
 Solid Grouting =
 Special Inspection =
 Modular Ratio 'n' =
 Short Term Factor =
 Equiv. Solid Thick. =
 Masonry Block Type = Medium Weight

Concrete Data

fc psi = 3,000.0
 Fy psi = 60,000.0

Other Acceptable Sizes & Spacings

Toe: Not req'd, Mu < S * Fr
 Heel: Not req'd, Mu < S * Fr
 Key: No key defined

Footing Design Results

	Toe	Heel
Factored Pressure	2,755	0 psf
Mu' : Upward	310	38 ft-#
Mu' : Downward	33	326 ft-#
Mu: Design	277	288 ft-#
Actual 1-Way Shear	0.00	4.93 psi
Allow 1-Way Shear	93.11	93.11 psi
Toe Reinforcing	# 4 @ 12.00 in	
Heel Reinforcing	# 4 @ 12.00 in	
Key Reinforcing	None Spec'd	



CHARLES WARREN ENGINEERING
 409 Montello Ave.
 Hood River, OR 97031
 (541) 386-1455

Title : Delaere Gaddis Place
 Job # : 29.05 Dsgnr: CW
 Page: _____
 Date: SEP 8, 2005
 Description....

4' HOUSE BASEMENT RETAINING WALL

This Wall in File: c:\rp6\projects\delaware gaddis place.rp5

RetainPro Version 6.0

Build Date : 10-SEP-2001, (c) 1989-2001

Cantilevered Retaining Wall Design

Summary of Overturning & Resisting Forces & Moments

ItemOVERTURNING.....			=RESISTING.....		
	Force lbs	Distance ft	Moment ft-#		Force lbs	Distance ft	Moment ft-#
Heel Active Pressure	= 519.7	1.58	819.5				
Toe Active Pressure	= -26.7	0.44	-11.9				
Surcharge Over Toe	=						
Adjacent Footing Load	=						
Added Lateral Load	=						
Load @ Stem Above Soil	=						
Total	= 493.1	O.T.M. =	807.6				
Resisting/Overturning Ratio		=	2.03				
Vertical Loads used for Soil Pressure	=	1,636.0 lbs					
Vertical component of active pressure NOT used for soil pressure							
Soil Over Heel	=	433.0	1.58			685.6	
Sloped Soil Over Heel	=						
Surcharge Over Heel	=						
Adjacent Footing Load	=						
Axial Dead Load on Stem	=	200.0	0.83			166.7	
Soil Over Toe	=	20.0	0.25			5.0	
Surcharge Over Toe	=						
Stem Weight(s)	=	583.0	0.83			485.8	
Earth @ Stem Transitions	=						
Footing Weight	=	300.0	1.00			300.0	
Key Weight	=						
Vert. Component	=						
Total	=	1,536.0 lbs	R.M.=			1,643.1	



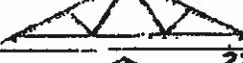
BATCHJOB: TL4525
 Date: 8/4/2005
 TRUSS SYSTEMS
 525 E. SOUTH HILL RD
 SUNNYSIDE, WA 98944
 1-888-836-2055
 Sales Rep: GARY
 Delivery date:
 Truck ID:
 Loaded by: Inspected by:

Reaction # TL4525
 TUM-A-LUM HR

Job: STEVE DALARRE
 WHITE SALMON

503-310-0319
 Loading: 55 7 10 24.00"O.C.

Permit required:

ITEM	QTY	TRUSS ID	SPAN		B1	B2	B3	B4	B5
1	1	AGB	31' 5" 0		React				
					Uplift				
					Horiz				
2	1	AGB1	31' 5" 0		React	2538	2262		
					Uplift	-587	-489		
					Horiz	76	76		
3	9	AT1	31' 5" 0		React	2538	2538		
					Uplift	-587	-587		
					Horiz	64	-64		
4	4	AT2	31' 5" 0		React	2115	2984		
					Uplift	-489	-742		
					Horiz	-83	-83		
5	10	AT3	31' 5" 0		React	2538	2262		
					Uplift	-587	-489		
					Horiz	75	75		
6	1	BGB	22' 3" 0		React				
					Uplift				
					Horiz				
7	12	BT1	22' 3" 0		React	1878	1878		
					Uplift	-477	-477		
					Horiz	64	64		



BATCHJOB: TL4525
 Date: 6/4/2005
 TRUSS SYSTEMS
 525 E. SOUTH HILL RD
 SUNNYSIDE, WA 98944
 1-888-836-2055
 Sales Rep: GARY
 Designer: LS
 Delivery date:

Invoice# TL4525
 TUM-A-LUM HR

page 1 of 1

GARY
 3-C

Job: STEVE DALARRE
 WHITE SALMON

503-310-0319

Loading: 55 7 10 24.00"O.C.

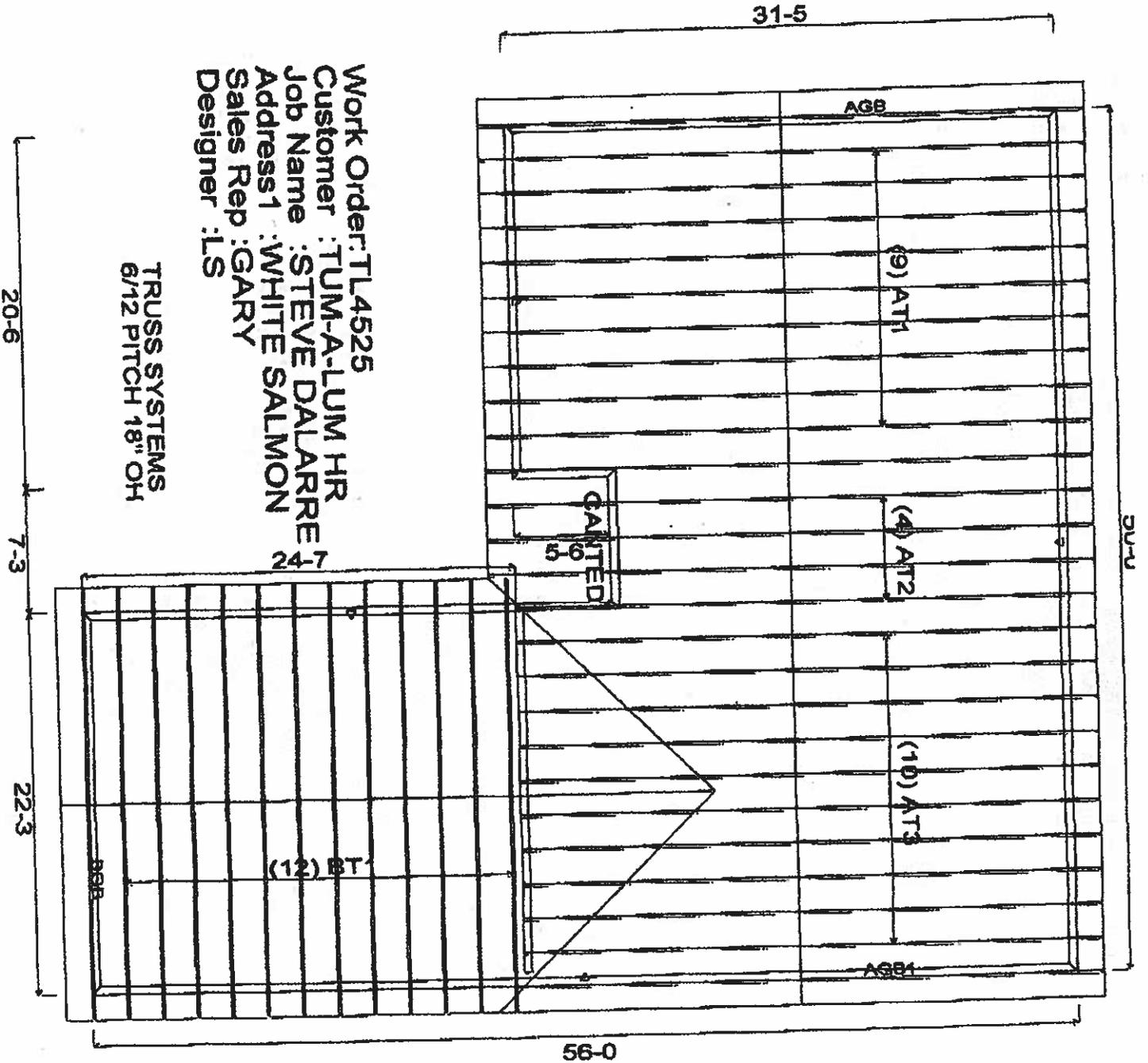
ITEM	QTY	TRUSS ID	SPAN	PITCH	OVERHANGS
1	1	AGB	31' 5" 0	6.00/0.00	18.00/ 18.00
2	1	AGB1	31' 5" 0	6.00/0.00	18.00/ 0.00
3	9	AT1	31' 5" 0	6.00/0.00	18.00/ 18.00
4	4	AT2	31' 5" 0	6.00/0.00	18.00/ 18.00
5	10	AT3	31' 5" 0	6.00/0.00	18.00/ 0.00
6	1	BGB	22' 3" 0	6.00/0.00	18.00/ 18.00
7	12	BT1	22' 3" 0	6.00/0.00	18.00/ 18.00

Terms:
 Past Due:

3986.00

MN/ N. AX

THXS LUDN



Work Order: TL4525
 Customer : TUM-A-LUM HR
 Job Name : STEVE DALARRE
 Address 1 : WHITE SALMON
 Sales Rep : GARY
 Designer : LS

TRUSS SYSTEMS
 6/12 PITCH 18" OH

R602.10.3 Braced wall panel construction methods. The construction of braced wall panels shall be in accordance with one of the following methods:

1. Nominal 1-inch-by-4-inch (25.4 mm by 102 mm) continuous diagonal braces let in to the top and bottom plates and the intervening studs or approved metal strap devices installed in accordance with the manufacturer's specifications. The let-in bracing shall be placed at an angle not more than 60 degrees (1.06 rad) or less than 45 degrees (0.79 rad) from the horizontal.
2. Wood boards of $\frac{5}{8}$ inch (15.9 mm) net minimum thickness applied diagonally on studs spaced a maximum of 24 inches (610 mm). Diagonal boards shall be attached to studs in accordance with Table R602.3(1).
3. Wood structural panel sheathing with a thickness not less than $\frac{5}{16}$ inch (7.9 mm) for 16-inch (406 mm) stud spacing and not less than $\frac{3}{8}$ inch (9.5 mm) for 24-inch (610 mm) stud spacing. Wood structural panels shall be installed in accordance with Table R602.3(3).
4. One-half-inch (12.7 mm) or $\frac{25}{32}$ -inch (19.8 mm) thick structural fiberboard sheathing applied vertically or horizontally on studs spaced a maximum of 16 inches (406 mm) on center. Structural fiberboard sheathing shall be installed in accordance with Table R602.3(1).
5. Gypsum board with minimum $\frac{1}{2}$ -inch (12.7 mm) thickness placed on studs spaced a maximum of 24 inches (610 mm) on center and fastened at 7 inches (178 mm) on center with the size nails specified in Table R602.3(1) for sheathing and Table R702.3.5 for interior gypsum board.
6. Particleboard wall sheathing panels installed in accordance with Table R602.3(4)
7. Portland cement plaster on studs spaced a maximum of 16 inches (406 mm) on center and installed in accordance with Section R703.6.
8. Hardboard panel siding when installed in accordance with Table R703.4.

Exception: Alternate braced wall panels constructed in accordance with Section R602.10.6 shall be permitted to replace any of the above methods of braced wall panels.

R602.10.4 Length of braced panels. For Methods 2, 3, 4, 6, 7 and 8 above, each braced wall panel shall be at least 48 inches (1219 mm) in length, covering a minimum of three stud spaces where studs are spaced 16 inches (406 mm) on center and covering a minimum of two stud spaces where studs are spaced 24 inches (610 mm) on center. For Method 5 above, each braced wall panel shall be at least 96 inches (2438 mm) in length where applied to one face of a braced wall panel and at least 48 inches (1219 mm) where applied to both faces.

Exceptions:

1. Lengths of braced wall panels for continuous wood structural panel sheathing shall be in accordance with Section R602.10.5.

2. Lengths of alternate braced wall panels shall be in accordance with Section R602.10.6.

R602.10.5 Continuous structural panel sheathing. When continuous wood structural panel sheathing is provided in accordance with Method 3 of R602.10.3 on all sheathable areas of all exterior walls, and interior braced wall lines, where required, including areas above and below openings, braced wall panel lengths shall be in accordance with Table R602.10.5. Wood structural panel sheathing shall be installed at corners in accordance with Figure R602.10.5. The bracing amounts in Table R602.10.1 for Method 3 shall be permitted to be multiplied by a factor of 0.9 for walls with a maximum opening height that does not exceed 85 percent of the wall height or a factor of 0.8 for walls with a maximum opening height that does not exceed 67 percent of the wall height.

R602.10.6 Alternate braced wall panels. Alternate braced wall lines constructed in accordance with one of the following provisions shall be permitted to replace each 4 feet (1219 mm) of braced wall panel as required by Section R602.10.4:

1. In one-story buildings, each panel shall have a length of not less than 2 feet, 8 inches (813 mm) and a height of not more than 10 feet (3048 mm). Each panel shall be sheathed on one face with $\frac{3}{8}$ -inch-minimum-thickness (9.5 mm) wood structural panel sheathing nailed with 8d common or galvanized box nails in accordance with Table R602.3(1) and blocked at all wood structural panel sheathing edges. Two anchor bolts installed in accordance with Figure R403.1(1) shall be provided in each panel. Anchor bolts shall be placed at panel quarter points. Each panel end stud shall have a tie-down device fastened to the foundation, capable of providing an uplift capacity of at least 1,800 pounds (816.5 kg). The tie-down device shall be installed in accordance with the manufacturer's recommendations. The panels shall be supported directly on a foundation or on floor framing supported directly on a foundation which is continuous across the entire length of the braced wall line. This foundation shall be reinforced with not less than one No. 4 bar top and bottom. When the continuous foundation is required to have a depth greater than 12 inches (305 mm), a minimum 12-inch-by-12-inch (305 mm by 305 mm) continuous footing or turned down slab edge is permitted at door openings in the braced wall line. This continuous footing or turned down slab edge shall be reinforced with not less than one No. 4 bar top and bottom. This reinforcement shall be lapped 15 inches (381 mm) with the reinforcement required in the continuous foundation located directly under the braced wall line.
2. In the first story of two-story buildings, each braced wall panel shall be in accordance with Item 1 above, except that the wood structural panel sheathing shall be provided on both faces, sheathing edge nailing spacing shall not exceed four inches on center, at least three anchor bolts shall be placed at one-fifth points, and tie-down device uplift capacity shall not be less than 3,000 pounds (1360.8 kg).

TABLE R602.10.1
WALL BRACING

SEISMIC DESIGN CATEGORY OR WIND SPEED	CONDITION	TYPE OF BRACE ^{b,c}	AMOUNT OF BRACING ^{a,d,e}
Categories A and B ($S_s \leq 0.35g$ and $S_{ds} \leq 0.33g$) or 100 mph and less	One story Top of two or three story	Methods 1, 2, 3, 4, 5, 6, 7 or 8	Located at each end and at least every 25 feet on center but not less than 16% of braced wall line.
	First story of two story Second story of three story	Methods 1, 2, 3, 4, 5, 6, 7 or 8	Located at each end and at least every 25 feet on center but not less than 16% of braced wall line for Method 3 and 25% of braced wall line for Methods 2, 4, 5, 6, 7 or 8.
	First story of three story	Methods 2, 3, 4, 5, 6, 7 or 8	Minimum 48-inch-wide panels located at each end and at least every 25 feet on center but not less than 25% of braced wall line for method 3 and 35% of braced wall line for Methods 2, 4, 5, 6, 7 or 8.
Category C ($S_s \leq 0.6g$ and $S_{ds} \leq 0.53g$) or less than 110 mph	One story Top of two or three story	Methods 1, 2, 3, 4, 5, 6, 7 or 8	Located at each end and at least every 25 feet on center but not less than 16% of braced wall line for Method 3 and 25% of braced wall line for Methods 2, 4, 5, 6, 7 or 8.
	First story of two story Second story of three story	Methods 2, 3, 4, 5, 6, 7 or 8	Located at each end and at least every 25 feet on center but not less than 30% of braced wall line for Method 3 and 45% of braced wall line for Methods 2, 4, 5, 6, 7 or 8.
	First story of three story	Methods 2, 3, 4, 5, 6, 7 or 8	Located at each end and at least every 25 feet on center but not less than 45% of braced wall line for Method 3 and 60% of braced wall line for Methods 2, 4, 5, 6, 7 or 8.
Category D ₁ ($S_s \leq 1.25g$ and $S_{ds} \leq 0.83g$) or less than 110 mph	One story Top of two or three story	Methods 2, 3, 4, 5, 6, 7 or 8	Located at each end and at least every 25 feet on center but not less than 20% of braced wall line for Method 3 and 30% of braced wall line for Methods 2, 4, 5, 6, 7 or 8.
	First story of two story Second story of three story	Methods 2, 3, 4, 5, 6, 7 or 8	Located at each end and not more than 25 feet on center but not less than 45% of braced wall line for Method 3 and 60% of braced wall line for Methods 2, 4, 5, 6, 7 or 8.
	First story of three story	Methods 2, 3, 4, 5, 6, 7 or 8	Located at each end and not more than 25 feet on center but not less than 60% of braced wall line for Method 3 and 85% of braced wall line for Method 2, 4, 5, 6, 7 or 8.
Category D ₂ or less than 110 mph	One story Top of two story	Methods 2, 3, 4, 5, 6, 7 or 8	Located at each end and at least every 25 feet on center but not less than 25% of braced wall line for Method 3 and 40% of braced wall line for Methods 2, 4, 5, 6, 7 or 8.
	First story of two story	Methods 2, 3, 4, 5, 6, 7 or 8	Located at each end and not more than 25 feet on center but not less than 55% of braced wall line for Method 3 and 75% of braced wall line for Methods 2, 4, 5, 6, 7 or 8.
	Cripple walls	Method 3	Located at each end and not more than 25 feet on center but not less than 75% of braced wall line.

For SI: 1 inch = 25.4 mm, 1 foot = 304.8 mm, 1 pound per square foot = 0.0479 kN/m², 1 mile per hour = 1.609 km/h.

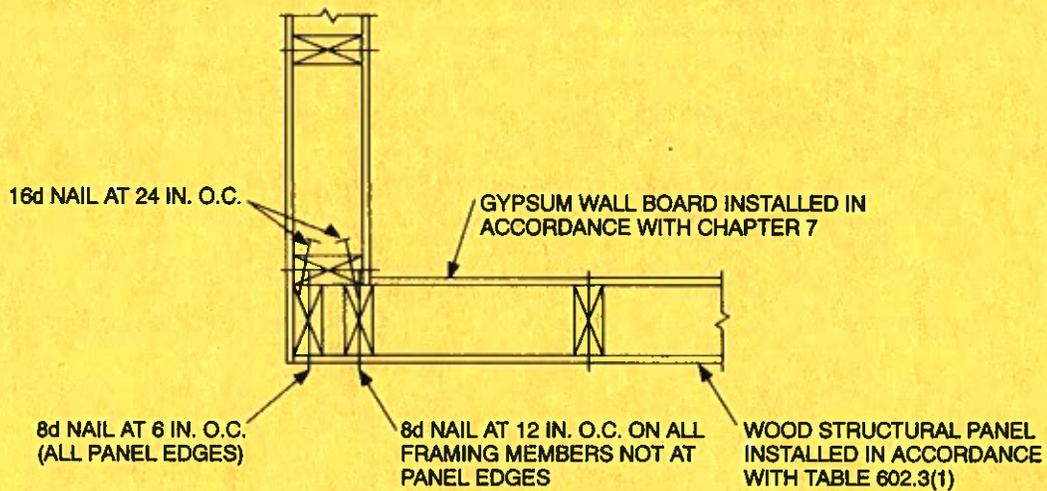
- Wall bracing amounts are based on a soil site class "D." Interpolation of bracing amounts between the S_{ds} values associated with the Seismic Design Categories shall be permitted when a site specific S_{ds} value is determined in accordance with Section 1615 of the *International Building Code*.
- Foundation cripple-wall panels shall be braced in accordance with Section R602.10.2.
- Methods of bracing shall be as described in Section R602.10.3. The alternate braced wall panels described in Section R602.10.6 shall also be permitted.
- The bracing amounts for Seismic Design Categories are based on a 15 psf wall dead load. For walls with a dead load of 8 psf or less, the bracing amounts shall be permitted to be multiplied by 0.85 provided that the adjusted bracing amount is not less than that required for the site's wind speed. The minimum length of braced panel shall not be less than required by Section R602.10.3.
- When the dead load of the roof/ceiling exceeds 15 psf, the bracing amounts shall be increased in accordance with Section R301.2.2.4. Bracing required for a site's wind speed shall not be adjusted.

TABLE R602.10.5
LENGTH REQUIREMENTS FOR BRACED WALL PANELS IN A CONTINUOUSLY SHEATHED WALL^{a,b}

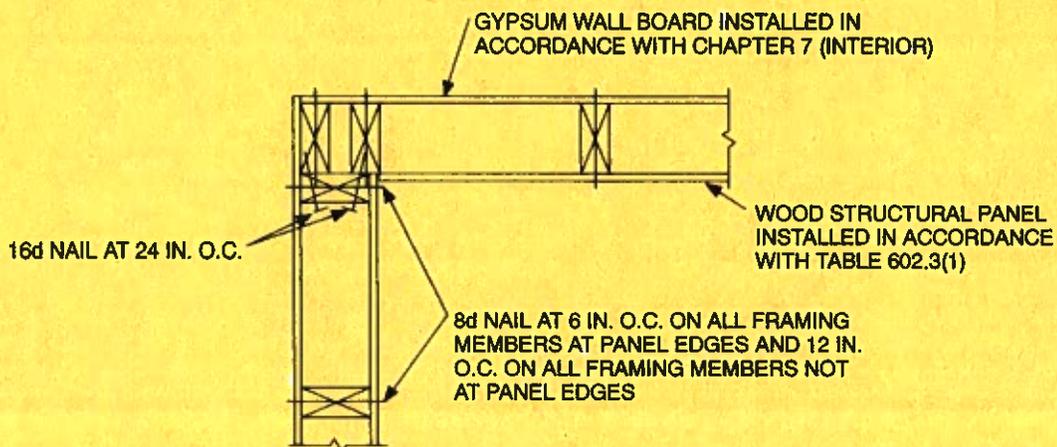
LENGTH OF BRACED WALL PANEL (Inches)			MAXIMUM OPENING HEIGHT NEXT TO THE BRACED WALL PANEL (% of wall height)
8-foot wall	9-foot wall	10-foot wall	
48	54	60	100%
32	36	40	85%
24	27	30	65%

For SI: 1 inch = 25.4 mm, 1 foot = 305 mm, 1 pound per square foot = 0.0479 kN/m².

- a. Linear interpolation shall be permitted.
- b. Full-height sheathed wall segments to either side of garage openings that support light frame roofs with roof covering dead loads of 3 psf or less shall be permitted to have a 4:1 aspect ratio.



(a) OUTSIDE CORNER DETAIL



(b) INSIDE CORNER DETAIL

For SI: 1 inch = 25.4 mm.

FIGURE R602.10.5
EXTERIOR CORNER FRAMING